Model-independent test of the truncated crater function theory of surface morphology evolution during ion bombardment

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A broad class of "local response" theories seeks to predict morphology evolution during energetic particle irradiation in terms of average surface height response to individual impacts—an approach that has been generalized by the crater function formalism of Norris *et al.* [J. Phys.: Condens. Matter 21, 224017 (2009); Nat. Commun. 2, 276 (2011)]. Keeping only the terms in the crater function formalism associated with the response of a flat surface has facilitated the use of molecular dynamics simulations of individual ion impacts to predict the stability or instability of a flat surface to ion bombardment. Here we report a sensitive experimental test of this truncated crater function theory that is independent of any *a priori* knowledge of the crater function itself. Existing measurements for 1 keV Ar⁺/Si and Kr⁺/Ge are inconsistent with the predictions of truncated crater function theory, for any conceivable crater function, at high bombardment angles. The failure of the theory suggests that the prediction of surface evolution from simulations of single-ion impacts will be more challenging than had been assumed.

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Energetic particle irradiation of solid surfaces can produce a variety of nanoscale surface topographies, including dots, ripples, holes, and ultrasmoothing [1]. The physical mechanisms governing this pattern formation are not yet well understood. The most widely investigated theoretical approaches to the phenomenon treat large-scale, long-time morphology evolution during bombardment as being due to the superposition of surface height changes associated with individual ion impacts. For simplicity, we call this broad class of theories "local response" theories. Seminal examples of local response theories are the Bradley-Harper (BH) [2] theory examining effects of erosion and the Carter-Vishnyakov (CV) [3] examination of "mass redistribution" (i.e., displacement of nearby atoms that are not eroded away). In their analyses the BH and CV theories used simple models for sputter erosion and atomic redistribution, respectively. More recently, Davidovitch et al. [4] showed that the surface morphology evolution can be sensitive to the details of the average local response to individual ion impacts rather than just its broad characteristics. Motivated by these results, Norris et al. [5,6] developed a general local response formalism predicting the surface evolution during ion bombardment from the moments of the crater function $\Delta h(x,y;\theta)$ —the average change in height of a flat surface at point (x,y) due to an ion impact at the origin. Here θ is the angle of ion incidence with respect to the surface normal. The crater function approach incorporates both erosive and redistributive effects, and reproduces the earlier BH and CV approaches when appropriate simple local responses are assumed [5]. A key practical goal of local response theories is to predict surface evolution during ion bombardment from knowledge of the average response to an individual impact; this can itself, in principle, be obtained from molecular dynamics (MD) simulations [6,7]. To facilitate

use of MD simulations in predicting surface behavior, a recent simplification of the general crater function formalism, which we term "truncated" crater function theory, assumes that knowledge of the crater function formed on a flat surface is sufficient to determine the surface stability/instability in the linear stability limit of infinitesimal perturbations from a smooth, flat surface [6,8]. Consequently, it expresses the curvature coefficients governing surface evolution in terms of only the angular dependence of the first moment of the crater function $M^{(1)}(\theta)$.

For the case of Ar^+ bombardment of Si (Ar^+/Si) , Norris *et al.* [6] used crater function moments calculated from MD simulations to correctly predict the $\theta \cong 45^\circ$ transition from stability to instability with increasing bombardment angle. In this case, they found that redistribution plays a much larger role in driving surface structure than does erosion, except possibly very near grazing incidence. This is consistent with recent *in situ* grazing incidence small-angle x-ray scattering (GISAXS) measurements of the curvature coefficients in this system [9,10].

A major challenge in evaluating the accuracy of the crater function approach is that experimental measurements of the crater function are unavailable and MD calculations of the function or its moments are computer-intensive and of uncertain accuracy. If a given crater function prediction made using input from MD is shown to be wrong, is the problem with the MD results or with the formalism itself? Here we point out that, independent of the shape of the crater function for a given system, the structure of the truncated form of Ref. [6] places strong constraints on the behavior of the curvature coefficients. Thus, measurements of the curvature coefficients as functions of ion incidence angle can provide sensitive tests of truncated crater function theory without *a priori* knowledge of the crater function or its moments.

Within linear theory, which describes surface morphology evolution at early times and low fluence, the evolution of surface height h(x,y,t) during ion bombardment can be

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written as [2]

$$\frac{\partial h(x,y,t)}{\partial t} = \left(S_X(\theta) \frac{\partial^2 h}{\partial x^2} + S_Y(\theta) \frac{\partial^2 h}{\partial y^2} \right) - B \nabla^4 h, \quad (1)$$

where $S_{X,Y}(\theta)$ are the curvature coefficients governing the long-wavelength (i.e., lengths on which a continuum description is accurate) behavior of the surface in the x direction (parallel to the projected direction of the ion beam, or "parallel mode") and y direction (perpendicular to the projected direction, or "perpendicular mode"). The coefficient B represents the magnitude of ion-enhanced surface-confined viscous flow, which is always a smoothing effect. In writing Eq. (1) we neglect for simplicity the average erosion rate and slope-dependent erosion rate, which do not affect the linear stability or instability of the surface: the erosion rate can be neglected by working in the frame of reference of the average surface height, and Fourier analysis following the methods of Ref. [9] reveals that the slope-dependent erosion rate contributes only an imaginary component (traveling waves) to the perturbation's amplification rate. When either $S_{X,Y}(\theta) > 0$, the surface is stable to long-wavelength fluctuations in that direction; conversely, when either $S_{X,Y}(\theta) < 0$ the surface is unstable to long-wavelength fluctuations in that direction.

The truncated crater function approach of Ref. [6] expands the local response in moments of the crater function; the first moment is simply $M^{(1)}(\theta) = \int x \Delta h(x, y; \theta) dx dy$. The theory predicts the angle-dependent curvature coefficients to be [6]

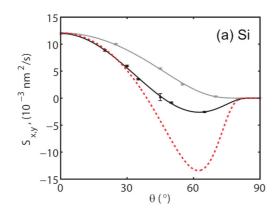
$$S_X(\theta) = I_0 \frac{d}{d\theta} [M^{(1)}(\theta) \cos(\theta)], \qquad (2)$$

$$S_Y(\theta) = I_0 M^{(1)}(\theta) \cos(\theta) \cot(\theta), \tag{3}$$

where I_o is the ion-beam flux.

We now examine constraining predictions introduced by the theoretical approach itself. By symmetry $M^{(1)}(\theta=0^\circ)=0$. Because we expect $M^{(1)}(\theta)$ to remain finite as $\theta\to 90^\circ$, the expression inside the derivative of Eq. (2) goes to zero at both $\theta=0^\circ$ and $\theta=90^\circ$. Therefore

$$\int_{0^{\circ}}^{90^{\circ}} S_X(\theta) d\theta = I_0 \left[M^{(1)}(\theta) \cos \theta \right]_{0^{\circ}}^{90^{\circ}} = 0.$$
 (4)



This is a strong constraint that is independent of the shape of the crater function itself. It states that no matter what the relative magnitudes of the contributions from erosive and redistributive effects are, there must be a properly weighted balance between regions of bombardment angles causing surface stability and instability.

A second constraint arises because both $S_V(\theta)$ and $S_V(\theta)$

A second constraint arises because both $S_X(\theta)$ and $S_Y(\theta)$ are functions of $M^{(1)}$. Therefore Eqs. (2) and (3) can be used to write $S_X(\theta)$ and $S_Y(\theta)$ in terms of each other:

$$S_Y(\theta) = \cot \theta \int_0^\theta S_x(q) dq \,; \tag{5}$$

$$S_X(\theta) = \frac{d}{d\theta}(S_y \tan \theta). \tag{6}$$

Independent measurements of the two curvature coefficients as functions of ion incidence angle can then be compared to this self-consistency requirement of the crater function theory.

To test the truncated crater function theory, we rely on recently published sets of $S_X(\theta)$ and $S_Y(\theta)$ values for 1-keV bombardment of Ar⁺/Si [9,10] and Kr⁺/Ge [11] using *in situ* GISAXS. Figures 1 and 2 reproduce the key experimental results for the angular dependence of the curvature coefficients. It is immediately clear that $\int_x^S(\theta) d\theta$ is not zero for either Ar⁺/Si or Kr⁺/Ge, in contrast to the prediction of the crater function theory. For Ar⁺/Si, the region of positive $S_X(\theta)$ is more than 3 times larger than the region of negative $S_X(\theta)$. For Kr⁺/Ge, which has a higher critical angle for the stability-instability transition, the asymmetry is even larger. Thus, in both cases there is a surfeit of stability as compared to instability.

We can obtain more information about where problems may lie by examining the predicted relationships of Eqs. (5) and (6). To do so, the experimental $S_{X,Y}(\theta)$ results must be parameterized. In Refs. [9] and [10] it was found that for Ar^+/Si the $S_{X,Y}(\theta)$ values could be fit well by a CV mass redistribution form: $S_X(\theta) \sim \cos 2\theta$; $S_Y(\theta) \sim \cos \theta$, modified with an empirical Yamamura correction factor $\exp[-\Sigma([1/\cos(\theta)] - 1)]$ [12]. The Kr^+/Ge results [11] are qualitatively similar to the Ar^+/Si results but with the transition angle from positive to negative $S_X(\theta)$ (i.e., from

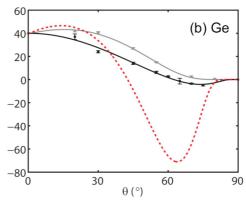


FIG. 1. (Color online) Data points: Experimental values of $S_X(\theta)$ (black circles) and $S_Y(\theta)$ (gray circles) as reported in (a) Refs. [9] and [10] for Ar⁺/Si and (b) Ref. [11] for Kr⁺/Ge. The black and gray lines are fits of the experimental $S_X(\theta)$ and $S_Y(\theta)$ to the heuristic functional forms of Eqs. (7) and (8). The red dashed lines are predictions of $S_X(\theta)$ from $S_Y(\theta)$ using Eq. (6). Positive values are stabilizing and negative values are destabilizing.

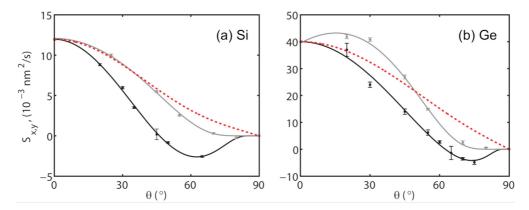


FIG. 2. (Color online) Data points: Experimental values of $S_X(\theta)$ (black circles) and $S_Y(\theta)$ (gray circles) as reported in (a) Refs. [9] and [10] for Ar⁺/Si and (b) Ref. [11] for Kr⁺/Ge. The black and gray lines are fits of the experimental $S_X(\theta)$ and $S_Y(\theta)$ to the heuristic functional forms of Eqs. (7) and (8). The red dashed lines are predictions of $S_Y(\theta)$ from $S_X(\theta)$ using Eq. (5). Positive values are stabilizing and negative values are destabilizing.

stability to instability) occurring at approximately 60° rather than 45°. Motivated by this observation, the incidence-angle dependence of the curvature coefficients for both ion and target combinations is here fit to a heuristic functional form:

$$S_X(\theta) = A\cos(\omega\theta)\exp\left(-\frac{B}{\cos\theta}\right).$$
 (7)

$$S_X(\theta) = A\cos(\omega\theta)\exp\left(-\frac{B}{\cos\theta}\right). \tag{7}$$

$$S_Y(\theta) = A\cos(\omega\theta + C)\exp\left(-\frac{B}{\cos\theta}\right). \tag{8}$$

The coefficients A, B, C, and ω are fitting parameters that are allowed to vary separately with each fit. The parameter C was added to Eq. (8) to address the observation that the maximum of the $S_{\gamma}^{\text{Ge}}(\theta)$ data occurs at 20° instead of 0°, which is unique to that data set. For Si, however, the CV-motivated part of the functional form, $\cos(\omega\theta + C)$, was found to have no effect on the fit of $S_Y^{Si}(\theta)$. Thus, ω and C were set to zero while fitting the $S_Y^{\text{Si}}(\theta)$ data. The resulting fits are shown in Figs. 1 and 2. The figures also contain the results of Eqs. (5) and (6), showing the calculated $S_X(\theta)$ (Fig. 1) and $S_Y(\theta)$ (Fig. 2) curves compared to the measured values. The values calculated in the fits are given in Table I.

The figures show, for both Ar⁺/Si and Kr⁺/Ge, a qualitative consistency between the measured curvature coefficients and those calculated from the opposite coefficient for bombardment angles below about 45°. At higher angles, the measured and calculated $S_X(\theta)$ curves are quite different. The $S_X(\theta)$ curve calculated from the curve-fitting experimental S_Y data exhibits much larger negative values (corresponding to greater predicted instability) than do the experimental $S_X(\theta)$ data. This is consistent with the conclusion drawn from examining the integral relationship above—the experimental $S_X(\theta)$ data are not as strongly negative as they would need to be in order to satisfy the consistency requirements of the existing crater function theory. Furthermore, it is clear that the critical angles of transition from stability to instability for 1 keV Ar⁺/Ge [13], Kr^+/Ge [14,11], and Kr^+/Si [15] are all well above 45°. These high transition angles suggest that there is indeed a surfeit of stability relative to instability compared to the prediction of crater function theory.

In contrast to the predicted behavior of $S_X(\theta)$, the measured and calculated $S_V(\theta)$ curves look reasonably similar even at high angles. We can understand this result from Eq. (5). As discussed above, the experimental $S_X(\theta)$ values clearly do not integrate to zero over the interval $[0^{\circ} - 90^{\circ}]$ as predicted by the crater function theory. Nonetheless, the impact of this behavior on the calculation of $S_Y(\theta)$ in Eq. (5) is modest because the $\cot(\theta)$ term forces the calculated $S_Y(\theta)$ to approach zero as $\theta \to 90^{\circ}$, even if the integral does not. Thus the qualitative behavior of the calculated $S_Y(\theta)$ curve is not strongly sensitive to the high-angle behavior of $S_X(\theta)$.

In summary, experimental results for 1 keV Ar⁺/Si and Kr⁺/Ge appear to show qualitative agreement with the predictions of the truncated crater function theory of Ref. [6] for bombardment angles less than approximately 45°. For angles well above this, the instability to parallel-mode ripple formation is far weaker than would be necessary to satisfy the predictions of the crater function approach for selfconsistency, for any conceivable crater function. It is unclear at present whether this discrepancy points to a fundamental problem with the assumptions (e.g., neglect of long-range effects such as stress generated by bombardment) that enter all local response theories or is instead a consequence of the simplifications made in assuming that only $M^{(1)}(\bar{\theta})$ contributes

TABLE I. Coefficient values, with 95% confidence bounds, calculated for the data sets used in this study using the fitting functions described in Eqs. (7) and (8).

	Fit of $S_{X,Si}$	Fit of $S_{Y,Si}$	Fit of $S_{X,Ge}$	Fit of $S_{Y,Ge}$
\overline{A}	25.43 ± 5.13	86.88 ± 17.51	58.67 ± 18.45	769.7 ± 29.6
B	0.7535 ± 0.181	1.973 ± 0.181	0.3827 ± 0.2763	1.934 ± 0.316
C	0	0	0	1.208 ± 0.109
ω	1.947 ± 0.05	0	1.441 ± 0.069	-0.253 ± 0.159

to the overall surface evolution. In either case, the use of MD simulations of individual ion impacts to predict overall surface evolution during ion bombardment will be more complicated than had been assumed—even in the linear stability limit of infinitesimal perturbations from a smooth, flat surface.

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